

9.1 ALTERNATIVE POST-INJECTION SITE CARE TIMEFRAME 40 CFR 146.93(a)

MARQUIS BIOCARBON PROJECT

Facility Information

Facility name: MARQUIS BIOCARBON PROJECT

Facility contact: ELIZABETH STEINHOOR
DIRECTOR OF ENVIRONMENTAL AFFAIRS
10000 MARQUIS DRIVE, HENNEPIN, IL 61327
815.925.7300 / BETHSTEINHOOR@MARQUISENERGY.COM

Well name: MCI CCS 3

Well location: PUTNAM COUNTY, ILLINOIS
Non Responsive -- Geological information

Table of Contents

9.1	Alternative Post-Injection Site Care and Site Closure (PISC) Plan.....	3
9.1.1	Computational Modeling Results – 40 CFR 146.93(c)(1)(i)	3
9.1.2	Predicted Timeframe for Pressure Decline – 40 CFR 146.93(c)(1)(ii)	5
9.1.3	Predicted Rate of Plume Migration – 40 CFR 146.93(c)(1)(iii)	5
9.1.4	Confining Zone Characterization – 40 CFR 146.93(c)(1)(vii)	5
9.1.5	Assessment of Fluid Movement Potential – 40 CFR 146.93(c)(1)(viii)-(ix).....	6
9.1.6	Location of USDWs – 40 CFR 146.93(c)(1)(x)	6
	References	8

List of Figures

Figure 9-1: Plot of porosity and permeability relationships for High Side Case (orange line) and Low Side Case (blue line). The numbers on the orange are permeability values, number on the blue line are porosity values. The porosity permeability relationship for the base case was calculated from the ratio between permeability and porosity at the intersection of the curves..... 4

Figure 9-2: CO₂ plume at layer 153 (used to delineate AoR) at the end of injection, 1, 5 and 10 years after injection stopped for the High Side Case (top row) and Low Side Case (bottom row).4

9.1 Alternative Post-Injection Site Care and Site Closure (PISC) Plan

Marquis Carbon Injection LLC will conduct post-injection monitoring for a five-year period following the cessation of injection operations. A justification for this alternative PISC timeframe is provided below.

9.1.1 Computational Modeling Results – 40 CFR 146.93(c)(1)(i)

Figure 9-3 in the PISC and Site Closure Plan (Permit Section 9) shows the cross section of the predicted CO₂ plume extent and demonstrates the CO₂ plume stability during alternative PISC timeframe. Figure 9-4 in the PISC and Site Closure Plan (Permit Section 9) illustrates a cross section of the predicted pressure front during the post-injection period. The pressure front declines quickly during the post-injection period. Figure 9-1 in the PISC and Site Closure Plan (Permit Section 9) shows, the predicted pressure at the MCI CCS 3 well reaches pre-injection pressure in less than the proposed 5-year PISC timeframe. Given the fast CO₂ plume stabilization and rapid pressure decrease in the Mt. Simon Sandstone predicted by the computational modeling, a 5-year PISC is appropriate to ensure USDW protection.

This was further supported by a sensitivity analysis to test the effects of varying the porosity and permeability relationships on the CO₂ plume shape and pressure behavior (Figures 9-1 and 9-2). High side and low side case runs, testing two porosity permeability relationships in addition to the base case were performed. The permeability vs porosity plot for each case in the Mt Simon is shown Figure 9-1. The results of the sensitivity analysis indicate that the CO₂ plume shape is similar in both cases compared to the base case scenario (Figure 9-2). Details related to this sensitivity analysis are discussed further in AoR and Corrective Action Plan Section (Permit Section 2.6.7).

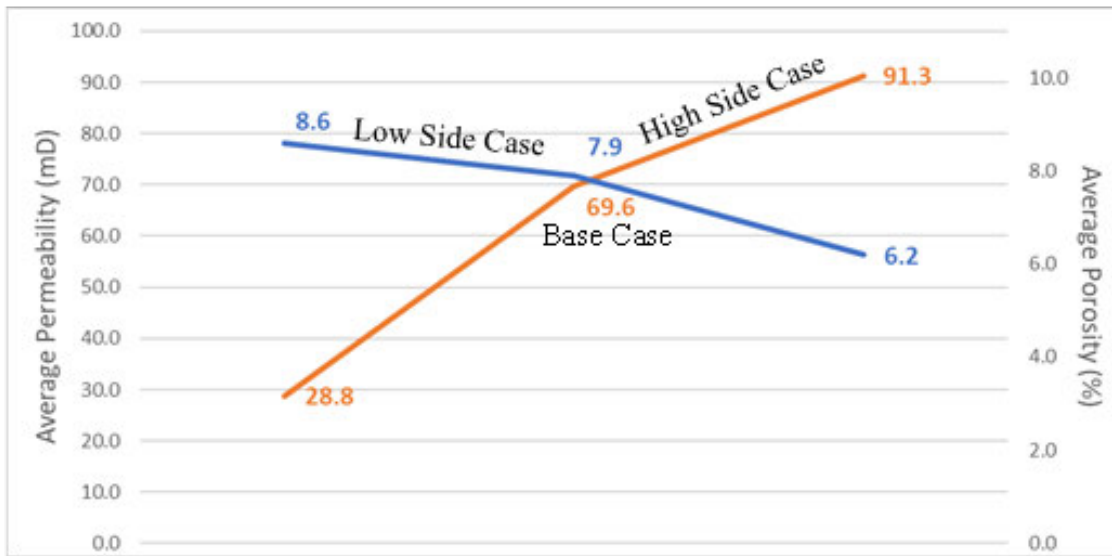


Figure 9-1: Plot of porosity and permeability relationships for High Side Case (orange line) and Low Side Case (blue line). The numbers on the orange are permeability values, number on the blue line are porosity values. The porosity permeability relationship for the base case was calculated from the ratio between permeability and porosity at the intersection of the curves.

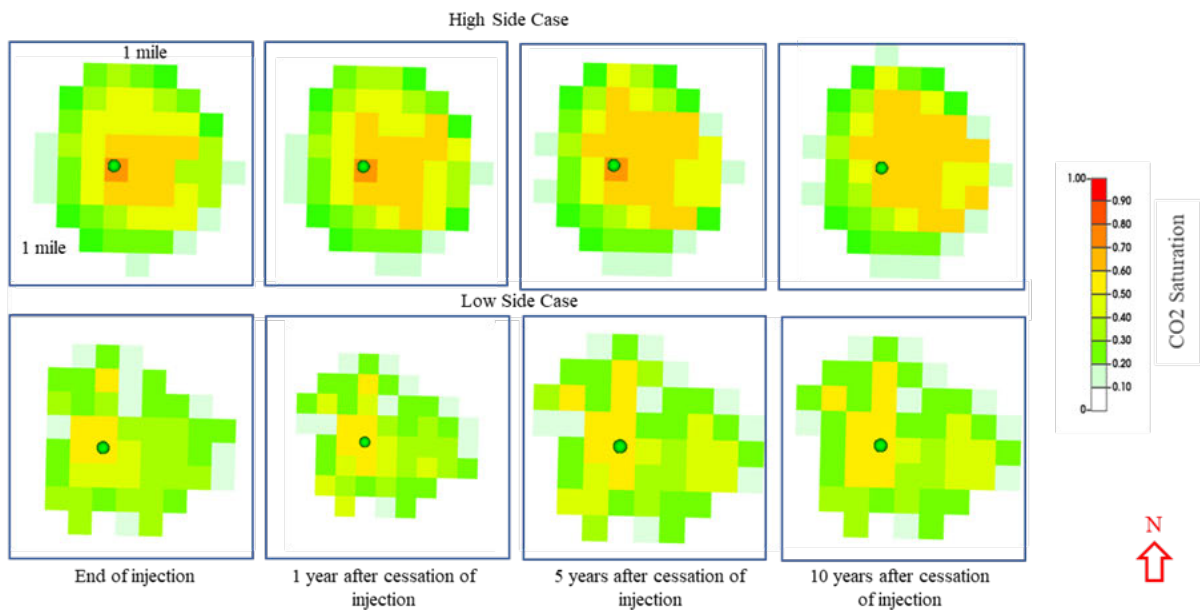


Figure 9-2: CO₂ plume at layer 153 (used to delineate AoR) at the end of injection, 1, 5 and 10 years after injection stopped for the High Side Case (top row) and Low Side Case (bottom row).

9.1.2 Predicted Timeframe for Pressure Decline – 40 CFR 146.93(c)(1)(ii)

Figure 9-4 in the PISC and Site Closure Plan (Permit Section 9) shows the cross section of the pressure front during the post injection phase. Additional plots and figures, showing the pressure front during the injection period, can be found in the AoR and Corrective Action Plan Section (Permit Section 2). The maximum spatial extent of the pressure front occurs at the end of the injection period. Figure 9-1 shows the predicted pressure buildup and decline at the MCI CCS 3 well through the injection phase and for 50 years of the post-injection period. The pressure declines immediately following cessation of injection and is predicted to be heterogenous between the MCI CCS 3 and MCI MW 2 wells. The details related to sensitivity analysis can be found in the AoR and Corrective Action Plan Section (Permit Section 2). A comparison of the pressure time series from the sensitivity analysis demonstrates that the pressure buildup during the injection phase and rapid decline during the PISC phase are similar to the base case scenario for different porosity permeability relationships.

Continuous pressure measurements will be acquired from the Mt. Simon Sandstone through the injection and PISC phases of the project (Testing and Monitoring Plan, Permit Section 7). The pressure data obtained during the injection phase of the project will be used to update the computational modelling every six months as per the reporting requirements in 40 CFR 146.91. Pressure data acquired during the PISC phase of the project are expected to verify the rapid decline in pressure in the Mt. Simon Sandstone predicted by the computational modelling.

9.1.3 Predicted Rate of Plume Migration – 40 CFR 146.93(c)(1)(iii)

Figure 9-2 shows the cross section of the CO₂ plume remains relatively stable from the end of the injection period to Year 3 and Year 5 of the PISC phase. Additional figures illustrating the predicted CO₂ plume expansion during the injection period are provided in the AoR and Corrective Action Plan Section (Permit Section 2.0). The average CO₂ plume extent was utilized to define the AoR. The details related to sensitivity analysis are presented in the AoR and Corrective Action Plan Section (Permit Section 2.6.7). The results from the sensitivity analysis show that the CO₂ plume shape remains a similar or smaller size and shape for the different modeled porosity permeability relationships (Figure 9-7).

9.1.4 Confining Zone Characterization – 40 CFR 146.93(c)(1)(vii)

The Eau Claire Formation is the primary confining unit for the project. The base of the Eau Claire Formation is comprised of the sandy Elmhurst Member where some CO₂ mobility is expected over time. However, the Eau Claire Formation has known thick and continuous shale intervals (Eau Claire Shale) above the Elmhurst Member, which have been confirmed as having good sealing capacity with core analysis (Permit Section 5). The Pre-Operational Testing Plan

details the characterization that has been completed for the Eau Claire Shale (Permit Section 5.0). This included assessing the mineralogy, geomechanics, and capillary pressure within the Eau Claire Shale.

The properties of the Eau Claire Formation were distributed within a static reservoir model and then imported into the computational model. Figure 9-3 shows the cross section of the plume map at the end of the injection period and for Years 3 and 5 of the PISC phase. Additional figures illustrating the CO₂ plume behavior during a 50-year post-injection period have been included in the AoR and Corrective Action Plan Section (Permit Section 2.0). Computational modeling results show that there would be no CO₂ penetration into the Eau Claire Shale during the injection and post-injection modeling period due to the low permeability of the Eau Claire Shale.

9.1.5 Assessment of Fluid Movement Potential – 40 CFR 146.93(c)(1)(viii)-(ix)

There is no evidence of geological conduits within the AoR. Also, within the AoR there are no existing wells that penetrate either the injection zone or the confining layer, so no corrective action is required.

The MCI CCS 3 well will be constructed according to the USEPA Class VI regulations, and several measures will be incorporated in the well design to ensure protection of the USDWs at the site following the injection period (Injection Well Construction Plan, Permit Section 4). The long casing string and packer will be constructed of corrosion-resistant alloys (CR13) across the injection reservoir and confining zone to reduce the chances of casing degradation over the long term. Similarly, a CO₂-resistant cement will be pumped behind the deep string casing across the injection reservoir and confining zone. Following completion of the injection phase of the project and monitoring efforts, the MCI CCS 3 well will be plugged and abandoned according to the EPA Class VI guidelines, including the use of CO₂-resistant cement across the storage formation (Injection Well Plugging Plan, Permit Section 8).

During the injection and PISC phases of the project, the well integrity of the injection and MCI MW 2 well will be monitored through several internal and external monitoring techniques (Section 9.3, Permit Section 7.0). Annular pressures and fluid volumes will be monitored in the MCI CCS 3 well on a continuous basis until the MCI CCS 3 well is abandoned. Annular pressures in the MCI MW 2 well will be monitored daily. Temperature logging is the primary external mechanical integrity test that will be used to monitor the MCI CCS 3 and MCI MW 2 wells on an annual basis.

9.1.6 Location of USDWs – 40 CFR 146.93(c)(1)(x)

At the Marquis BioCarbon Project site, the Mt. Simon Sandstone is not considered a USDW based on salinity samples acquired from MCI MW 1 with total dissolved solids (TDS)

concentrations greater than 10,000 milligrams per liter (mg/L) or 10,000 parts per million (ppm). The lowermost USDW is defined locally as the Gunter Sandstone of the Prairie du Chien Group (Knox Supergroup). At the MCI MW 1 well, the base of the Gunter Sandstone is 963 feet (ft) above the top of the Mt. Simon. USDWs in the project site range from the Gunter Sandstone (deepest USDW) to shallow, near-surface glacial till aquifers.

References

- Enick RM, Klara SM. CO₂ solubility in water and brine under reservoir conditions. Chemical Engineering Communications 90(1):23-33 (1990).
- FutureGen Alliance, 2013, Underground Injection Control Permit Applications for FutureGen 2.0 Morgan County Class VI UIC Wells 1, 2, 3, and 4, FG-RPT-017.
- Golden StrataServices, 1984, Jones & Laughlin Steel Inc, Hennepin Illinois, UIC Permit Application, UIC-004-WI-JL, EPA Facility ID No. ILD000781591.
- Land CS. Calculation of imbibition relative permeability for two-and three-phase flow from rock properties. Society of Petroleum Engineers Journal 8(02):149-56 (1968).
- Li YK, Nghiem LX. Phase equilibria of oil, gas and water/brine mixtures from a cubic equation of state and Henry's law. The Canadian Journal of Chemical Engineering 64(3):486-96(1986).
- Nghiem L, Shrivastava V, Tran D, Kohse B, Hassam M, Yang C. Simulation of CO₂ storage in saline aquifers. In: SPE/EAGE Reservoir Characterization & Simulation Conference: European Association of Geoscientists & Engineers. p. cp-170-00063 (2009).
- Raziperchikolaee S, Alvarado V, Yin S. Effect of hydraulic fracturing on long-term storage of CO₂ in stimulated saline aquifers. Applied energy 102:1091-104 (2013).